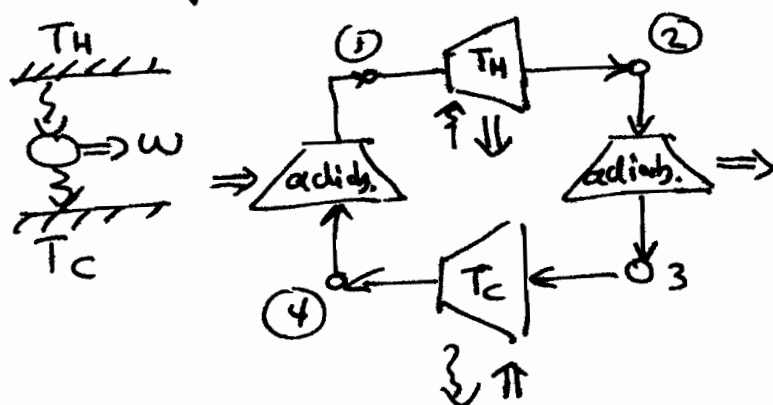


Ch. 4 Power Generation + Cooling

How are power generation / refrigeration cycles implemented in practice?

Ideal-Gas Heat Engines

(not practical, but instructional to analyze)

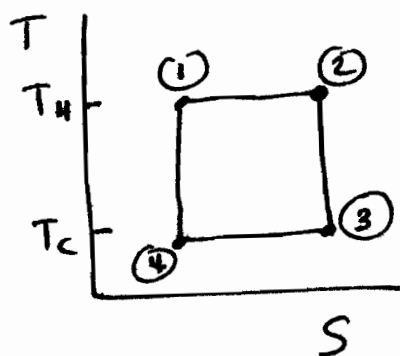


① → ② isoth. expansion, T_H

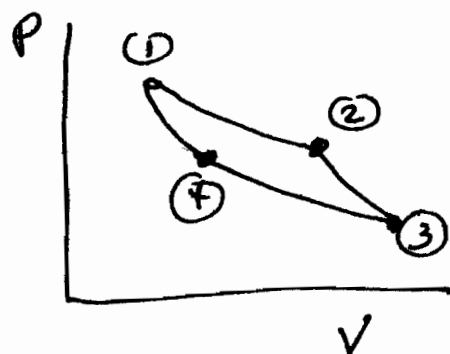
② → ③ adiab. compression

③ → ④ isoth. compression T_C

④ → ① adiab. compression



↻ power generation
↻ cooling



When analyzed using
adiabatic ideal gas
expressions + 1st Law
balances (see
Example 4.1)

$$\Rightarrow \eta = \frac{-W}{Q_H} = \frac{T_H - T_C}{T_H}$$

Theoretical maximum
(Carnot) efficiency

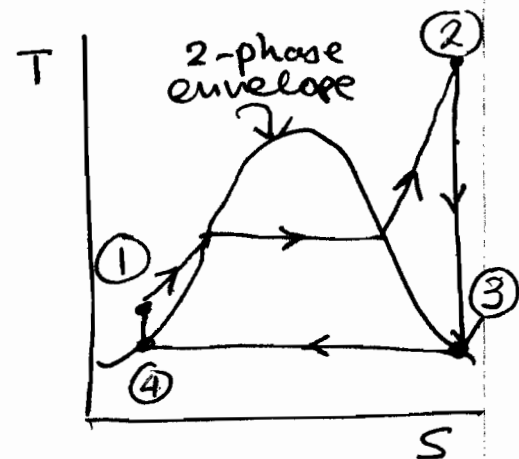
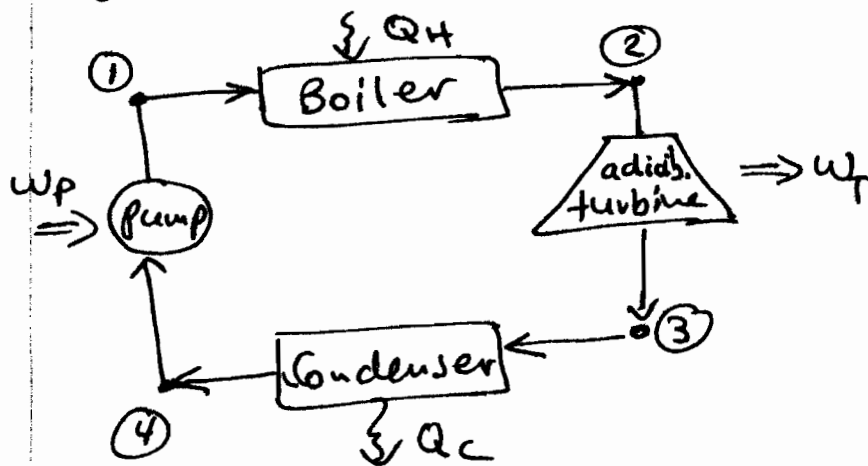
∴ Ideal-gas T is the same as Carnot T
⇒ Thermodynamic Temperature

Practical issues preventing implementation:

- * Isothermal turbines/compressors cannot be constructed
- * Need huge equipment sizes (low p of I.G.)
- * Cost of compression

Rankine Cycle

Practical power generation using a working fluid (usually steam). Industrial Revolution.



Example 4.2

Steam, $T_H = 800\text{ K}$, $T_C = 373\text{ K}$ $\eta = ?$

Start from point ③, saturated vapor @ $T_C = 373\text{ K}$

From WebBook } $P_3 = P_4 = 1\text{ bar}$ $\underline{H}_3 = 48.2 \frac{\text{kJ}}{\text{mol}}$ $\underline{S}_3 = 132.5 \frac{\text{J}}{\text{mol K}}$
 saturation T calc. } $\underline{H}_4 = 7.5 \frac{\text{kJ}}{\text{mol}}$ $\underline{S}_4 = 23.5 \frac{\text{J}}{\text{mol K}}$

Adiabatic expansion is - in the best case - isentropic, $\underline{S}_2 = \underline{S}_3$. From $T_2 = 800\text{ K}$ (isoth. calc.) we can obtain $P_2 = 27.4\text{ bar}$, $\underline{H}_2 = 63.4 \frac{\text{kJ}}{\text{mol}}$

The pumping step $(4) \rightarrow (1)$ also operates - at best - isentropically, so that: $\underline{S}_1 = \underline{S}_4 = 23.5 \frac{\text{J}}{\text{mol K}}$; from isobaric calculation at $P_1 = P_2 = 27.4 \text{ bar}$:

$$T_1 = 373 \text{ K (no T change)} \quad \underline{H}_1 = 7.6 \text{ kJ/mol}$$

$$\therefore \dot{W}_p = \underline{H}_1 - \underline{H}_4 = 0.1 \frac{\text{kJ}}{\text{mol}} \quad (\text{very small})$$

$$\dot{W}_T = \underline{H}_3 - \underline{H}_2 = -15.2 \frac{\text{kJ}}{\text{mol}} \quad \left. \vphantom{\dot{W}_T} \right\} \eta = \frac{15.2}{55.8} = 27\%$$

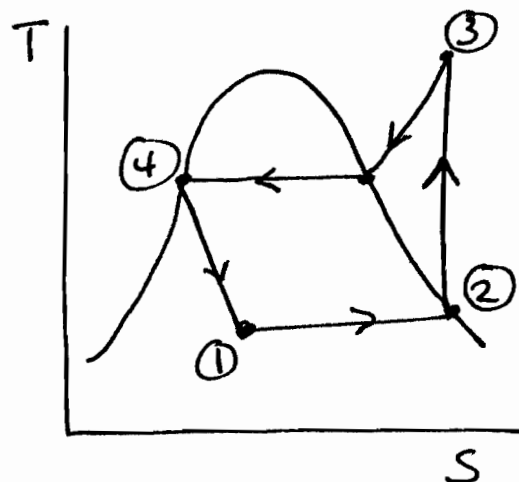
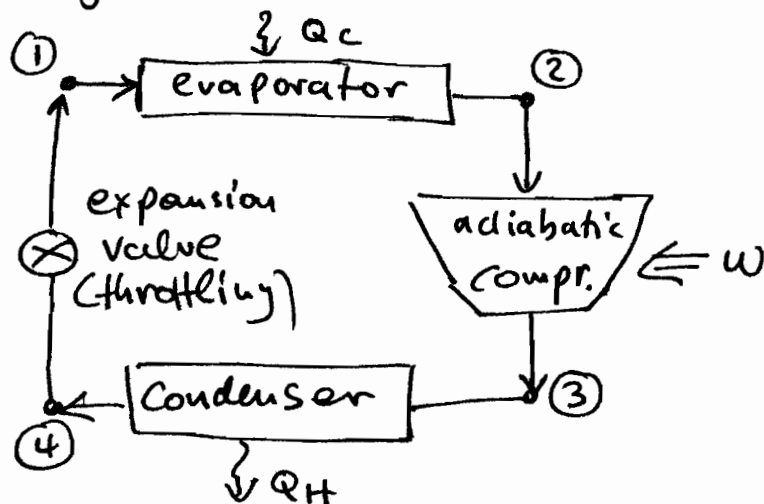
$$\dot{Q}_H = \underline{H}_2 - \underline{H}_1 = 55.8 \text{ kJ/mol}$$

Compare to $\eta_{\text{rev}} = \frac{800 - 373}{800} = 53\%$

Why is efficiency lower than Carnot? \rightarrow Non-isothermal operation of boiler

Refrigeration Cycles

Slight modification of "reversed" Rankine Cycle:



E.g. Car air conditioner w/ R134a (Example 4.3)

$$\theta_4 = 130^\circ \text{F}, \quad \theta_1 = \theta_2 = 40^\circ \text{F}$$

From the NIST WebBook, saturation properties of R134a @ 40°F , vapor: $\underline{H}_2 = 401 \frac{\text{kJ}}{\text{kg}}$ $\underline{S}_2 = 1.72 \frac{\text{J}}{\text{kg K}}$

Point ③ has $\underline{S}_3 = \underline{S}_2$

At $\theta_4 = 130^\circ\text{F}$, sat. liquid $\Rightarrow P_4 = 14.7 \text{ bar}$, $\underline{H}_4 = 279 \frac{\text{kJ}}{\text{kg}}$

Isobaric calculation at $P_3 = P_4$ to match the value of the entropy (1.72 J/kg K) gives:

$$\theta_3 = 137^\circ\text{F}, \quad \underline{H}_3 = 430 \frac{\text{kJ}}{\text{kg}}$$

Throttling valve is isenthalpic, $\underline{H}_1 = \underline{H}_4$

$$\dot{W} = \dot{H}_3 - \dot{H}_2 = 29 \frac{\text{kJ}}{\text{kg}} \quad \dot{Q}_c = \dot{H}_2 - \dot{H}_1 = 122 \frac{\text{kJ}}{\text{kg}}$$

$$J = \frac{122}{29} = 4.2$$

Compare to Carnot: $J^{\text{rev}} = \frac{T_c}{T_h - T_c} = 5.6$

With the use of two 3-way valves, the role of cold + hot coil can be reversed and an air conditioner can operate as a heat pump, bringing heat into a building from the outside (colder) air.